Kinematics & Dynamics of Linkages Lecture 10 – Geometric Linkage Synthesis



Spring 2018



Chapter Objectives

- 1. How to design a linkage that delivers a desired output
- 2. Types of linkages synthesis
- 3. Limitation of linkages synthesis
- 4. Geometric synthesis







Types of Synthesis

Path Generation

- Control of a **point** in the plane such that it follows some prescribed **path**
- No orientation control to the link that contains the point of interest

Motion Generation

- Control of a line in the plane such that it assumes some sequential set of prescribed positions
- **Orientation** of the link containing the line is important



Linkage Synthesis – Precision Points

- The points prescribed for successive locations of the output link
- Limited by the number of equations available
- Four bar linkage may have up to 5 precision points
- Usually, we use 2 or 3 precision points
 - Reduces to a set of linear simultaneous equations
 - More than 3 points requires complex software
- The solutions provide no guarantee as to the location of a linkage between precision points.



Linkage Synthesis – Verification

- Linkage synthesis procedures often provide solutions at the specified locations but not necessary in between these locations
- They say nothing about the linkage's behaviors between those positions
- It is possible that the resulting linkage will be incapable of moving from one precision point to another due to some constraint:
 - Toggle position
 - Transmission angle



Linkage Synthesis – Toggle Positions

You need to check that the linkage can reach all of the specified design positions without encountering a toggle position.



Non-Grashof: Triple rocker (Should be Avoided)

Grashof: Crank rocker

Slide 7 of 45

Linkage Synthesis – Transmission angle

The angle between the output link and the coupler should be a minimum μ > 40° (optimum 90°)



Slide 8 of 45

Geometric Linkage Synthesis – Case 1 2-Position Rocker Output

Design a four bar Grashof crank-rocker speed motor input to give 45° of rocker motion with equal time forward and back, from a constant speed motor input.





Draw the chord $B_1\!B_2$ and extended it in either direction.





Select a convenient point \boldsymbol{D}_2 on the line $\boldsymbol{B}_1\boldsymbol{B}_2$ extended.





Bisect line segment B_1B_2 , draw a circle of that radius about D_2 and label the two intersection of the circle and B_1B_2 extended, A_1 and A_2





Measure ground length 1, crank length 2, and rocker length 4.







Step 5: Check the Grashof condition and redo steps 2 to 5 with O_2 further from O_4 if non-Grashof.

Step 6: Build the linkage model and check its function and transmission angles.



- Rocker Output-Two Position with Complex Displacement (Motion)
- Design a four bar linkage to move link CD from C_1D_1 to C_2D_2 .





Draw construction line from point $\rm C_1$ to $\rm C_2$ and from point $\rm D_1$ to $\rm D_2$





Bisect line C_1C_2 and line D_1D_2 and extend their perpendicular bisectors to intersect at D_4 . Their intersection is the rotopole.





Select a convenient radius and draw an arc about the rotopole to intersect both lines O_4C_1 and O_4C_2 . Label the intersection B_1 and B_2 .





Steps 4-5: Repeat steps 4 and 5 of previous procedure **Step 6:** Make a model of the linkage and articulate it to check its function and its transmission angles





Design a fourbar linkage to move link CD from C_1D_1 to C_2D_2 (with moving pivots at C and D).





Draw construction line from point C_1 to C_2 and from point D_1 to D_2 .





Bisect line C_1C_2 and line D_1D_2 and extend their perpendicular bisectors in convenient directions. The rotopole will not be used in this solution.



MEE341 – Lecture 10: Geometric Linkage Synthesis

Slide 22 of 45 🛛 🔍 LAU

Select any convenient point on each bisector as the fixed pivots ${\rm O}_2$ and ${\rm O}_4$, respectively.



Slide 23 of 45

Step 4:

Connect D_2 with C_1 and call it link 2. Connect D_4 with D_1 and call it link 4.

Step 5:

Line C₁D₁ is link 3. Line O₂O₄ is link 1.

Step 6:

Check the Grashof condition, and repeat steps 3 to 6 if unsatisfied.





Make a model of the linkage and articulate it to check its function and its transmission angles





Combining Cases 1 and 3

Design a dyad to control and limits the extremes of motion of the linkages in the previous example to its two design positions



MEE341 – Lecture 10: Geometric Linkage Synthesis

Slide 26 of 45 🔝 LAU

Design a four–bar Grashof linkage that moves C-D from the first position C_1D_1 to C_2D_2 and then to the position C_3D_3







Draw construction lines from point $\rm C_1$ to $\rm C_2$ and from $\rm C_2$ to $\rm C_3$





Bisect line C_1C_2 and line C_2C_3 and extend their perpendicular bisector until they intersect. Label their intersection O_2 .





Repeat steps 2 and 3 for lines D_1D_2 and D_2D_3 . Label the intersection D_4 .





Connect D_2 with C_1 and call link 2. Connect D_4 with D_1 and call link 4. Line C_1D_1 is link 3. Line D_2D_4 is link 1.



MEE341 – Lecture 10: Geometric Linkage Synthesis

Slide 31 of 45 🔝 LAU

Step 5: Check the Grashof condition

Step 6: Construct Model and check toggle and transmission angles

Step 7: Construct Driver Dyade Link 3 C_1 Link 3 C_2 C_3 C_3 $Link 1 = O_2O_4$ **Non-Grashof**



Geometric Linkage Synthesis – Case 5 3-Position Motion Generation – Alternate Attachment Points

• Change the length of Link 3







Design a four bar linkage which move the link CD shown from position C_1D_1 to C_2D_2 and then to position C_3D_3 . Use specified fixed pivots D_2 and D_4 .





Draw construction arc from point C₂ to O₂ and from D₂ to O₂ whose radii define the side of triangle C₂O₂D₂. This defines the relationship of the fixed pivot O₂ to the coupler line CD in the second coupler position.





Draw construction arc from point C_2 to O_4 and from D_2 to O_4 whose radii define the side of triangle $C_2O_4D_2$. This defines the relationship of the fixed pivot O_4 to the coupler line CD in the second coupler position.





Now transfer this relationship back to the first coupler position C_1D_1 so that the ground plane position $D_2'D_4'$ bears the same relationship to C_1D_1 as D_2D_4 bore to the second coupler position C_2D_2 . We have inverted the problem.





Repeat the process for the third coupler position as shown in the figure and transfer the third relative ground link position to the first, or reference, position





The three inverted position of the ground plane that correspond to the three desired coupler positions are labeled $D_2 D_4, D_2' D_4'$, and $D_2'' D_4''$ and have also been renamed $E_1 F_1$, $E_2 F_2$ and $E_3 F_3$ as shown in the figure





Find rotopoles G and H





Connect G with E_1 and call it link 2. Connect H with F_1 and call it link 4. Line E_1F_1 is the coupler, link 3. Line GH is the ground link 1.





The figure shows the re-inversion of the linkage in which points G and H are now the moving pivots on the coupler and E_1F_1 has resumed its real identity as ground link D_2D_4





Reintroduce the original line C_1D_1 in its correct relationship to line D_2D_4 at the initial position as shown in the original example. This form the coupler plane and defines a minimal shape of link 3.





The angular motions required to reach the second and third position of line CD shown in the figure are the same as those defined in figure b for the linkage inversion





Step 9: Check the Grashof condition

Step 10: Construct a model and check toggle and transmission



